

# MEM 255 Introduction to Control Systems: *Modeling & analyzing systems*

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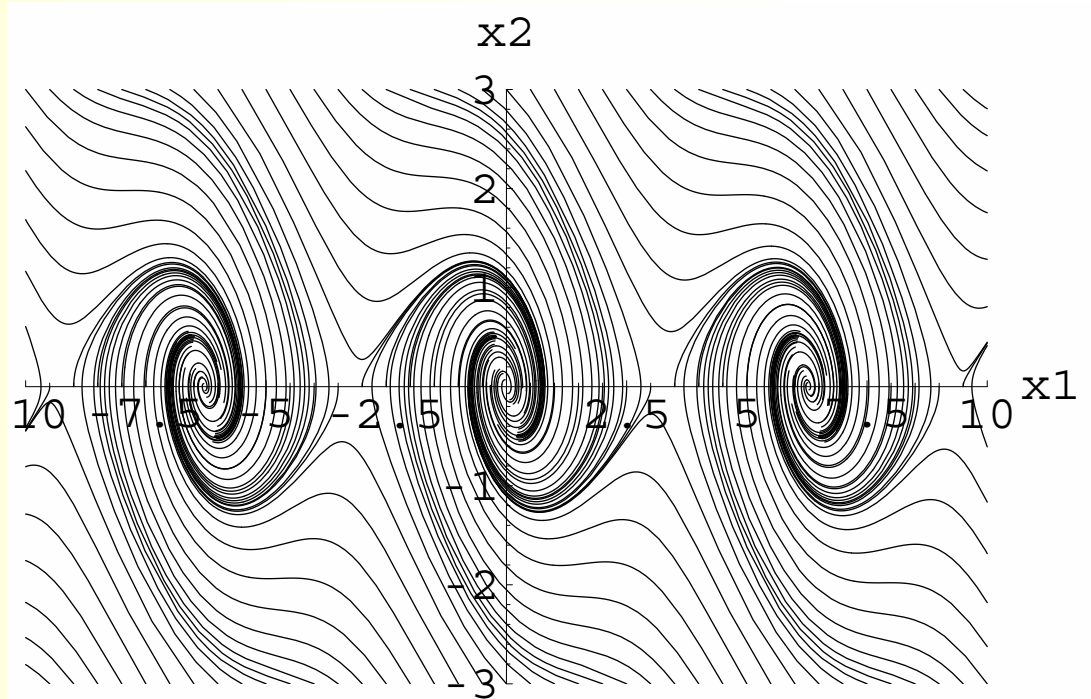
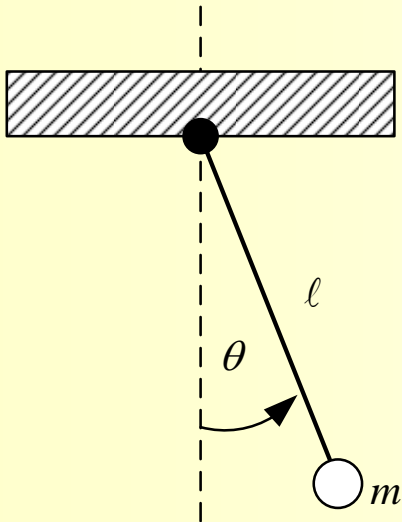
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# Outline

- **The Pendulum**
- **Micro-machined capacitive accelerometer**
  - **Differential equation model**
  - **Static (equilibrium) behavior**
  - **Dynamic behavior**
- **Linearizing Nonlinear Models**
- **Transfer Functions**
- **Using MATLAB numerics for solving odes**
- **Using MATLAB to compute the transfer function**

# Pendulum



$$ml^2\ddot{\theta} = -mgl \sin \theta - c\dot{\theta} + T(t)$$

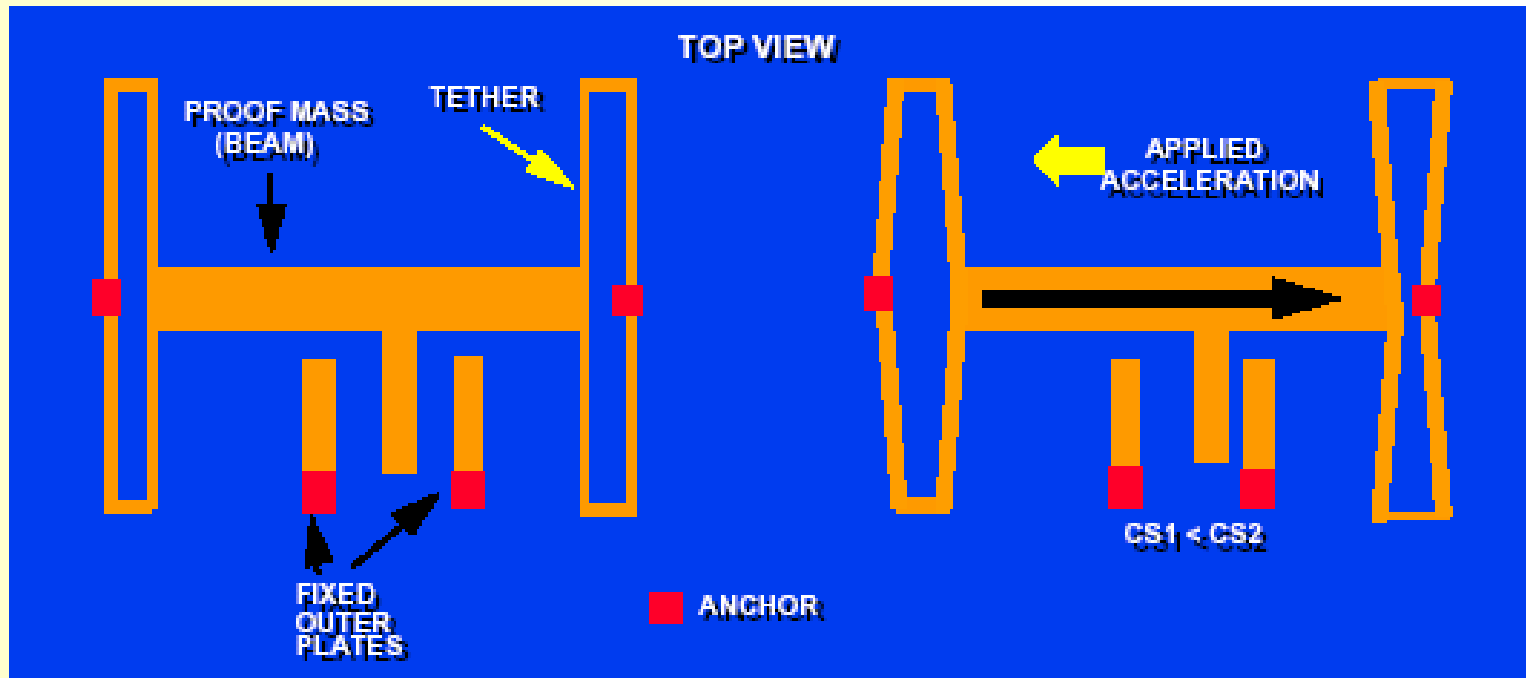
$$x_1 \triangleq \theta, x_2 \triangleq \dot{\theta} \Rightarrow$$

$$\dot{x} = f(x, u)$$

$$\dot{x}_1 = x_2$$

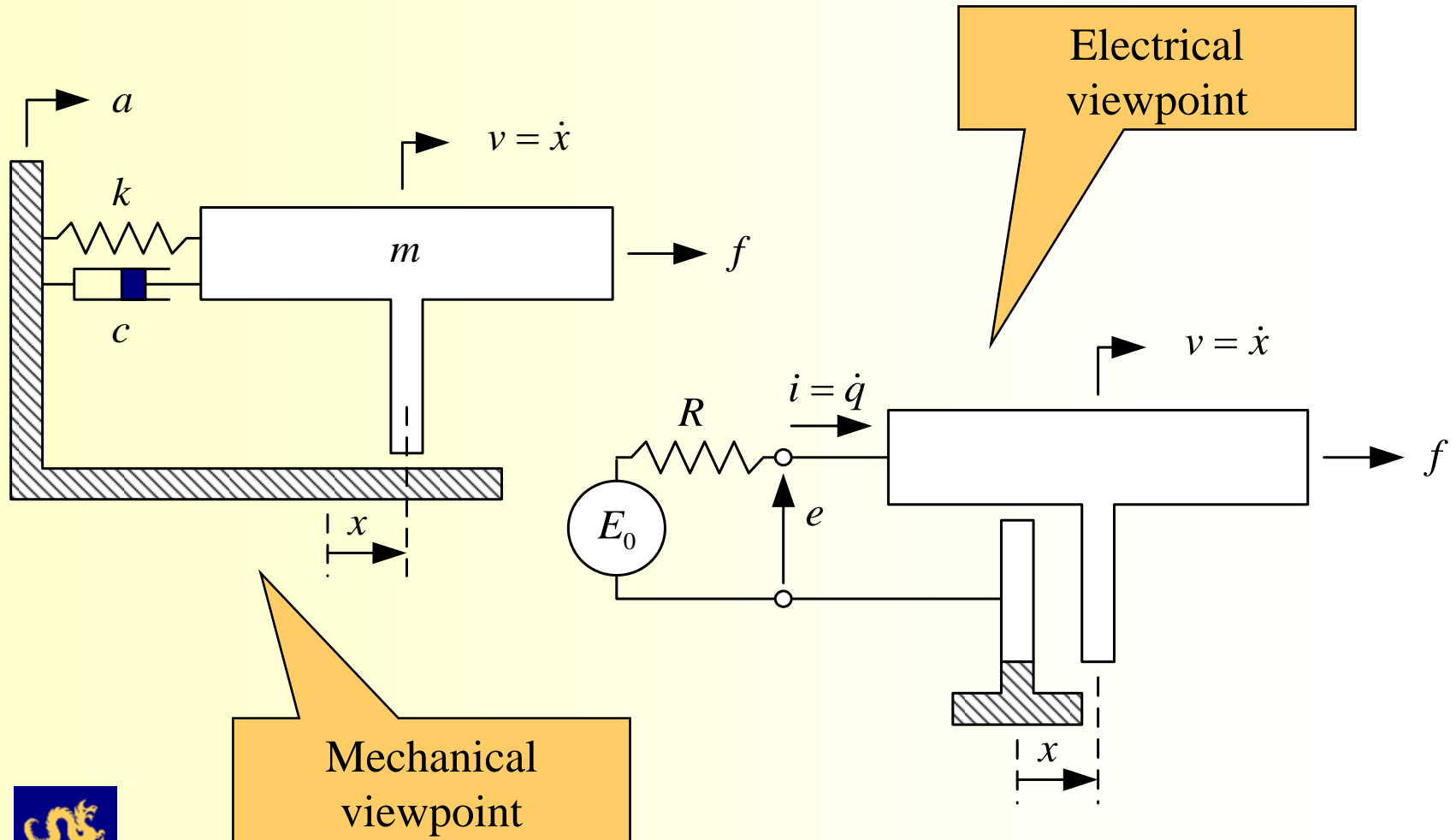
$$\dot{x}_2 = -(g/l)\sin x_1 - (c/ml^2)x_2 + (1/ml^2)T(t)$$

# Micro-machined Capacitive Accelerometer



From James Doscher, Analog Devices

# Accelerometer Model



# Governing Equations

$$m(\ddot{x} + a) = f - kx - c\dot{x} \Rightarrow m\ddot{x} = f - kx - c\dot{x} - ma \quad (\sum \text{Forces on } m)$$

$$E_0 = Ri + e \Rightarrow R\dot{q} + \frac{q}{C(x)} = E_0 \quad (\sum \text{Voltages around loop})$$

$$f = -\frac{q^2}{2C(x)^2} \frac{dC(x)}{dx}, \quad C(x) = C_0 \frac{d_0}{d_0 + x} \Rightarrow -\frac{1}{C(x)^2} \frac{dC(x)}{dx} = \frac{1}{C_0 d_0}$$

$$\dot{x} = v$$

$$\dot{v} = -\frac{q^2}{2m C_0 d_0} - \frac{k}{m} x - \frac{c}{m} v - a(t)$$

$$\dot{q} = -\frac{q(d_0 + x)}{RC_0 d_0} + \frac{1}{R} E_0$$

First order system of ODEs  
independent variable:  $t$   
states:  $x, v, q$  (dependent variables)  
input:  $a(t)$   
parameters:  $m, c, k, d_0, R, C_0, E_0$

# Remarks on Capacitor

Electric power supplied to capacitor:  $ei$

Mechanical power supplied to capacitor:  $fv$

Total work on capacitor:  $W = ei dt + fv dt = e dq + f dx$

Constitutive relation (electrically linear):  $q = C(x)e$

The electric energy stored in capacitor is defined by

$$dE_e(q, x) = e dq + f dx \Rightarrow$$

$$E_e = \int_0^q \frac{q}{C(x)} dq = \frac{q^2}{2C(x)}$$

$$e = \frac{\partial E_e}{\partial q} = \frac{q}{C(x)}, \quad f = \frac{\partial E_e}{\partial x} = -\frac{q^2}{2C(x)^2} \frac{dC(x)}{dx}$$

# Analyzing Ordinary Differential Equations

State vector

Input

Initial condition

system of first order odes:  $\dot{x} = f(x, u(t)), x(t_0) = x_0$

- Steady-state (equilibrium) behavior
  - Set input equal to a constant
  - Set state time derivative (velocity) equal to zero
- Dynamic behavior
  - Time response to initial conditions
  - Time response to inputs



# Equilibrium Behavior

$$0 = v$$

$$0 = -\frac{q^2}{2m C_0 d_0} - \frac{k}{m} x - \frac{c}{m} v - \bar{a} \Rightarrow$$

$$0 = -\frac{q(d_0 + x)}{RC_0 d_0} + \frac{1}{R} E_0$$

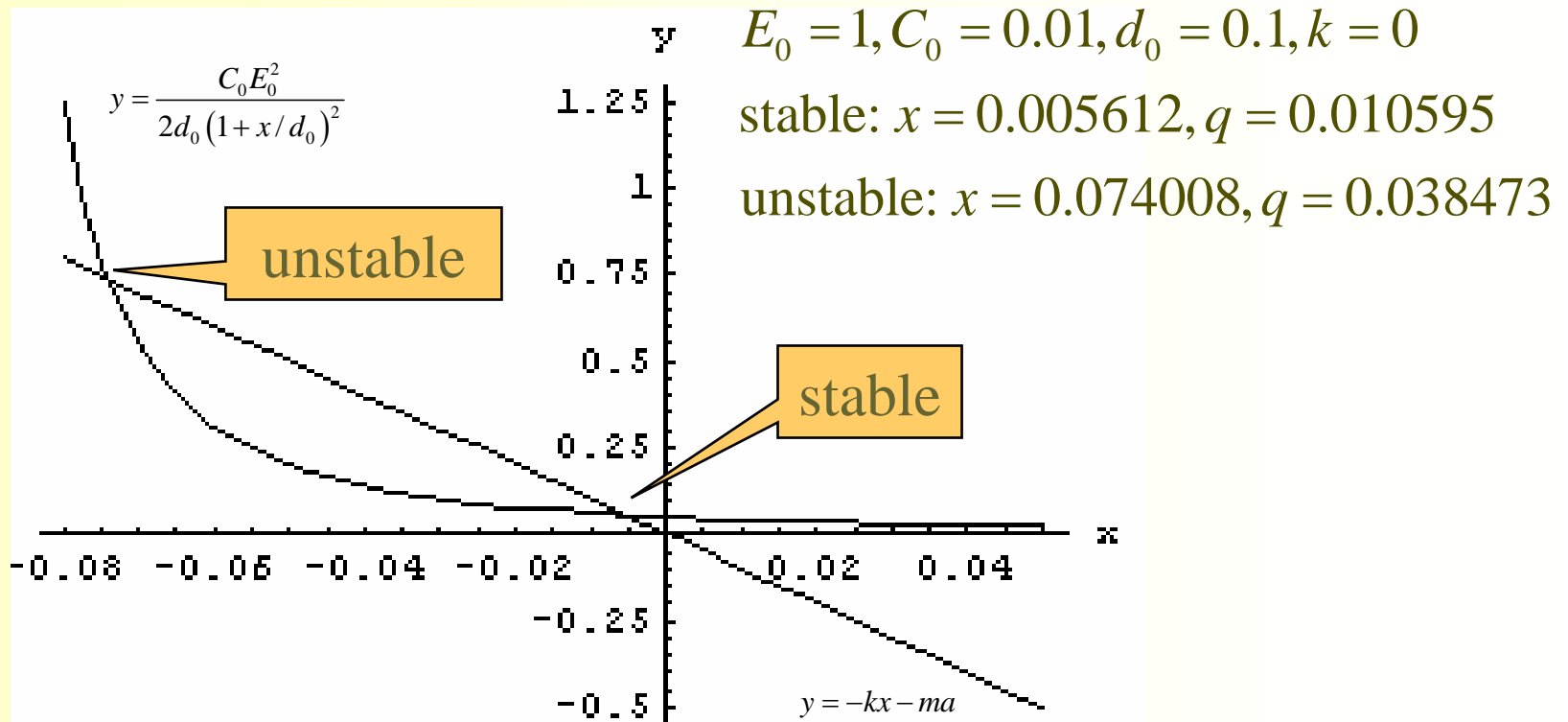
$$0 = -\frac{q^2}{2C_0 d_0} - kx - m\bar{a}$$

$$0 = -\frac{q(d_0 + x)}{C_0 d_0} + E_0$$

$$-kx - m\bar{a} = \frac{C_0 E_0^2}{2d_0 (1 + x/d_0)^2}$$

 eliminate  $q$

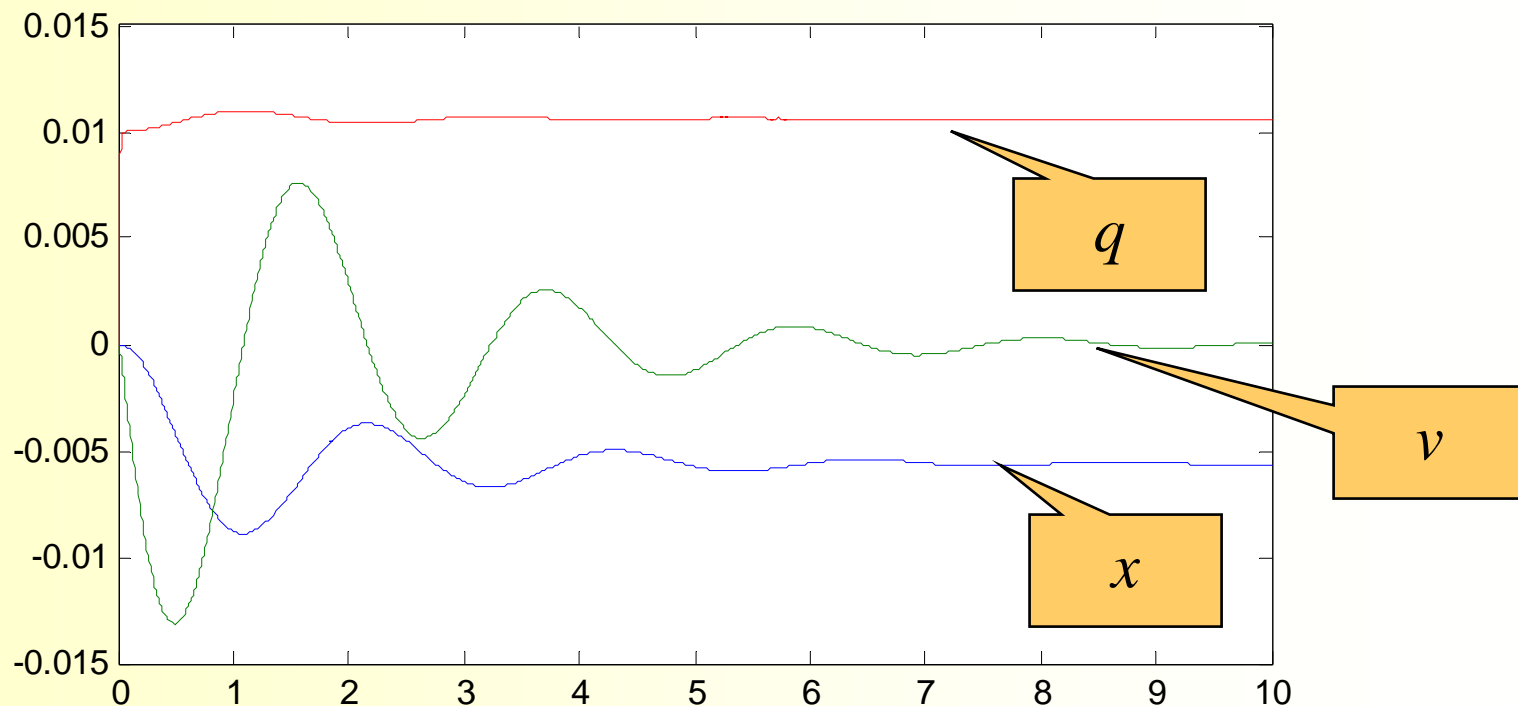
# Equilibrium Behavior



# Dynamic Behavior

Transient response from the origin:  $x(0) = 0, v(0) = 0, q(0) = 0$

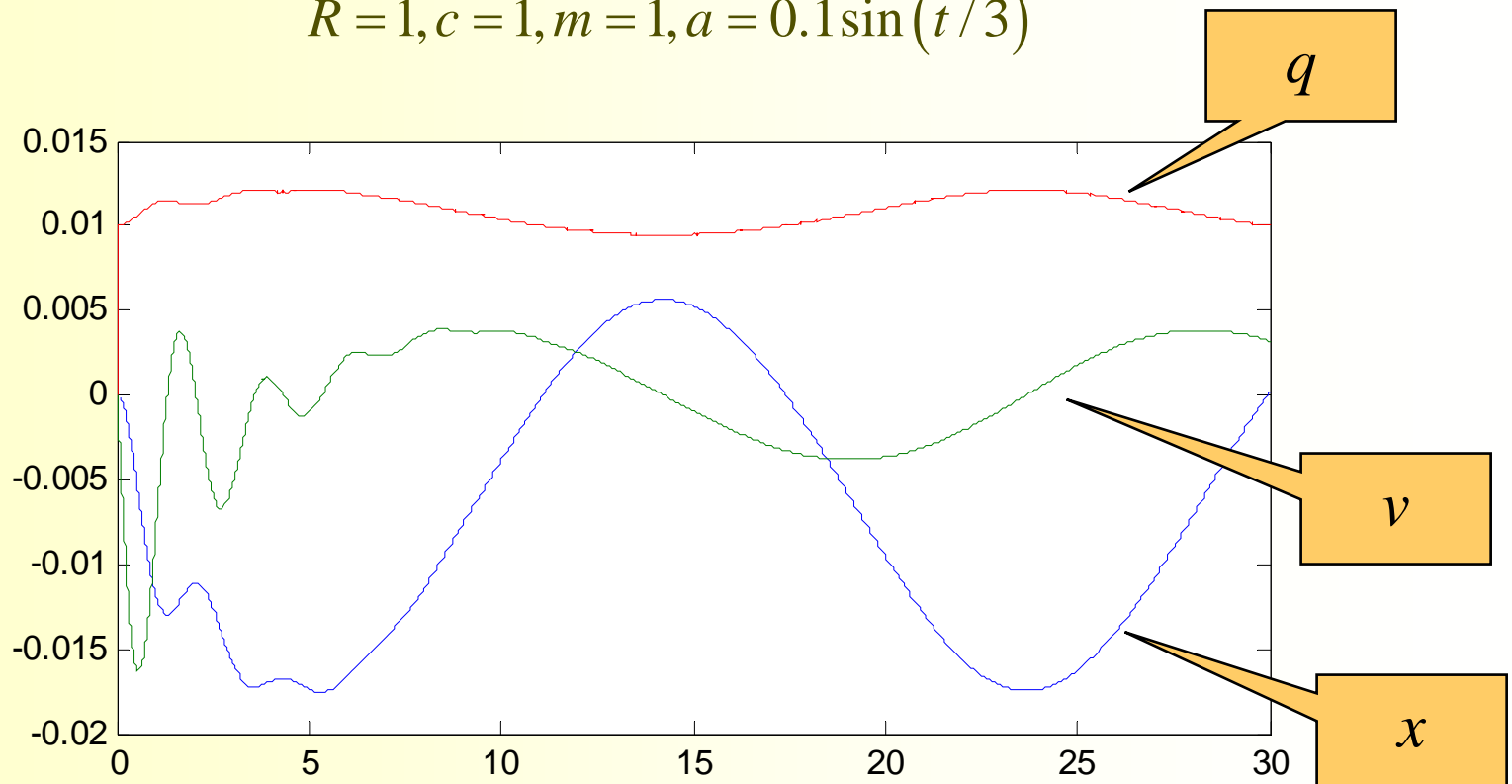
$$R = 1, c = 1, m = 1, a = 0$$



# Dynamic Behavior

Transient response from the origin:  $x(0) = 0, v(0) = 0, q(0) = 0$

$$R = 1, c = 1, m = 1, a = 0.1 \sin(t/3)$$



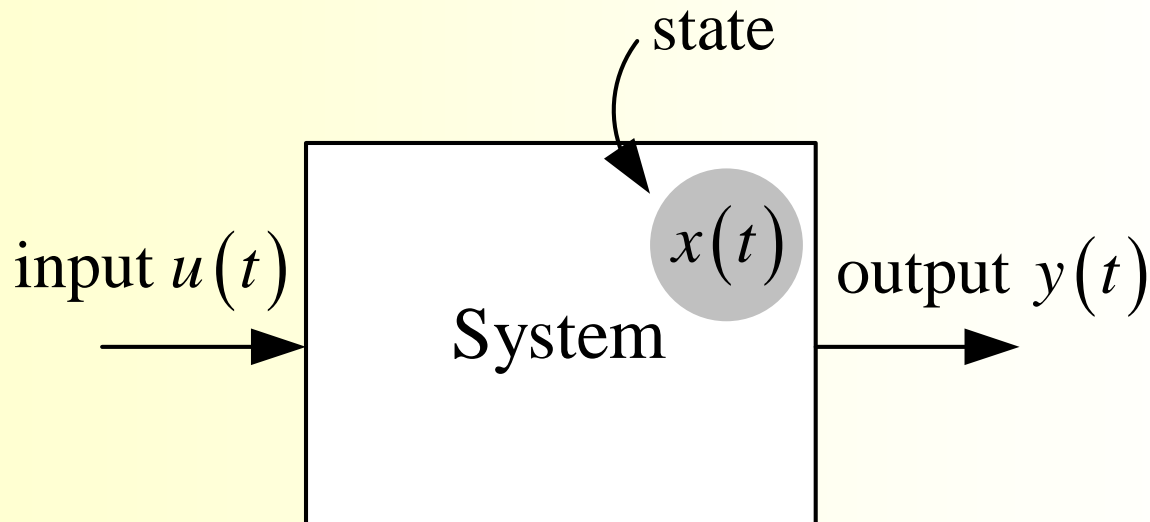
# Solving ODEs

```
function dy = accel(t,y)
dy = zeros(3,1);    % a column vector
a=0;
dy(1) = y(2);
dy(2) = -y(3)^2/0.002-10*y(1)-1*y(2)-a;
dy(3) = -y(3) * (0.1+y(1))/0.001+1;
```

Write a function that defines the differential equations

```
>> options = odeset('RelTol',1e-4,'AbsTol',[1e-4 1e-4 1e-5]);
>> [T,Y] = ode45(@accel,[0 10],[0 0 0],options);
>> plot(T,Y(:,1),T,Y(:,2),T,Y(:,3))
```

# General Model of Nonlinear System



$$\dot{x} = f(x, u) \quad \text{state equation}$$

$$y = h(x, u) \quad \text{output equation}$$

$$x \in R^n, u \in R^m, y \in R^q$$

# Linearization 1

In general models derived from physical principles involve sets of first and second order differential equations. These are reduced to first order standard form, involving the state vector  $x$ , input vector  $u$ , and output vector  $y$ .

$$\dot{x} = f(x, u) \text{ state equations}$$

$$y = h(x, u) \text{ output equations}$$

A set of values  $(x_0, u_0, y_0)$  is called an equilibrium point if they satisfy:

$$0 = f(x_0, u_0)$$

$$y_0 = h(x_0, u_0)$$

We are interested in motions that remain close to the equilibrium point.



# Linearization 2

Define:  $x(t) = x_0 + \delta x(t)$ ,  $u(t) = u_0 + \delta u(t)$ ,  $y(t) = y_0 + \delta y(t)$

$$\delta \dot{x} = f(x_0 + \delta x(t), u_0 + \delta u(t))$$

The equations become:

$$y_0 + \delta y(t) = h(x_0 + \delta x(t), u_0 + \delta u(t))$$

Now, construct a Taylor series for  $f, h$

$$f(x_0 + \delta x, u_0 + \delta u) = f(x_0, u_0) + \frac{\partial f(x_0, u_0)}{\partial x} \delta x + \frac{\partial f(x_0, u_0)}{\partial u} \delta u + \text{hot}$$

$$h(x_0 + \delta x, u_0 + \delta u) = h(x_0, u_0) + \frac{\partial h(x_0, u_0)}{\partial x} \delta x + \frac{\partial h(x_0, u_0)}{\partial u} \delta u + \text{hot}$$

Notice that  $f(x_0, u_0) = 0$  and  $h(x_0, u_0) = y_0$ , so

$$\delta \dot{x} = \frac{\partial f(x_0, u_0)}{\partial x} \delta x + \frac{\partial f(x_0, u_0)}{\partial u} \delta u$$

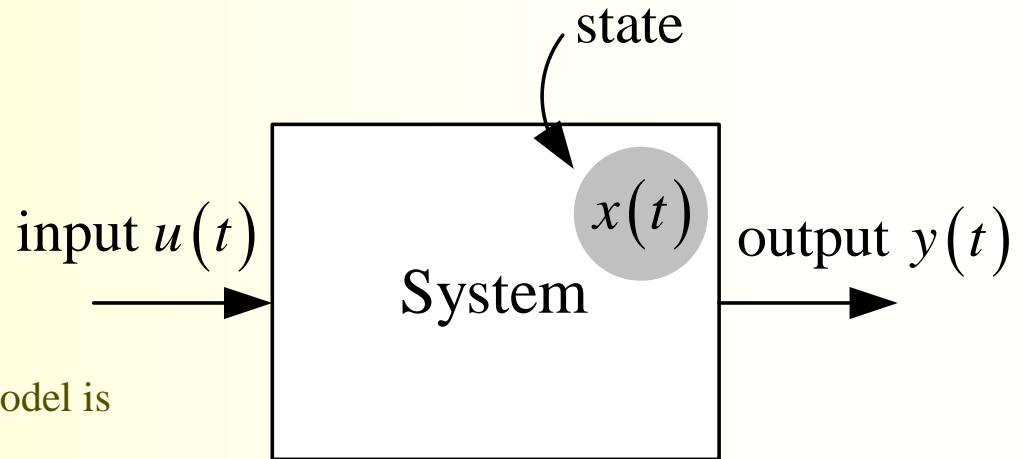
$$\delta y = \frac{\partial h(x_0, u_0)}{\partial x} \delta x + \frac{\partial h(x_0, u_0)}{\partial u} \delta u$$

$\Rightarrow$

$$\begin{array}{l} \delta \dot{x} = A\delta x + B\delta u \\ \delta y = C\delta x + D\delta u \end{array}$$



# Linear System Models: state space & transfer function



The differential equation or 'state space' model is

$$\begin{aligned}\dot{x}(t) &= Ax(t) + Bu(t) && \text{state equation} \\ y(t) &= Cx(t) + Du(t) && \text{output equation} \\ x(0) &= x_0 && \text{initial condition}\end{aligned}$$

The state space model describes how the input  $u(t)$  and the initial condition affect the state  $x(t)$  and the output  $y(t)$ . The 'transfer function' model is

$$Y(s) = G(s)U(s)$$

where  $Y(s), U(s)$  are the Laplace transforms of the output and input and  $G(s)$  is the transfer function.

The transfer function model describes how the input affects the output.

# Solving ODEs via the Laplace Transform

$$\dot{x} = Ax + Bu, \quad y = Cx + Du$$

$$\begin{aligned} \mathcal{L}(\dot{x}) &= A\mathcal{L}(x) + B\mathcal{L}(u) & \Rightarrow & \quad sX(s) - x_0 = AX(s) + BU(s) \\ \mathcal{L}(y) &= C\mathcal{L}(x) + D\mathcal{L}(u) & & \quad Y(s) = CX(s) + DU(s) \end{aligned}$$

$$X(s) = [sI - A]^{-1} x_0 + [sI - A]^{-1} BU(s)$$

$$Y(s) = C[sI - A]^{-1} x_0 + \left\{ C[sI - A]^{-1} B + D \right\} U(s)$$

Initial condition response

Input response

Transfer function:

$$G(s) = C[sI - A]^{-1} B + D$$

# Example: Accelerometer

$$\dot{x} = v$$

$$\dot{v} = -\frac{q^2}{2m} \frac{1}{C_0 d_0} - \frac{k}{m} x - \frac{c}{m} v - a(t) \quad e = -\frac{q(d_0 + x)}{C_0 d_0}$$

$$\dot{q} = -\frac{q(d_0 + x)}{RC_0 d_0} + \frac{1}{R} E_0$$

$$\delta \dot{x} = \delta v$$

$$\delta \dot{v} = -\frac{q_0}{m} \frac{1}{C_0 d_0} \delta q - \frac{k}{m} \delta x - \frac{c}{m} \delta v - \delta a(t)$$

$$\dot{q} = -\frac{(d_0 + x_0)}{RC_0 d_0} \delta q - \frac{q_0}{RC_0 d_0} \delta x$$

$$\delta e = -\frac{(d_0 + x_0)}{C_0 d_0} \delta q - \frac{q_0}{C_0 d_0} \delta x$$

# Example: Accelerometer

$$\begin{bmatrix} \delta \dot{x} \\ \delta \dot{v} \\ \delta \dot{q} \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 \\ -\frac{k}{m} & -\frac{c}{m} & -\frac{q_0}{m} \frac{1}{C_0 d_0} \\ -\frac{q_0}{RC_0 d_0} & 0 & -\frac{(d_0 + x_0)}{RC_0 d_0} \end{bmatrix} \begin{bmatrix} \delta x \\ \delta v \\ \delta q \end{bmatrix} + \begin{bmatrix} 0 \\ -1 \\ 0 \end{bmatrix} \delta a$$

$$\delta e = \begin{bmatrix} -\frac{q_0}{C_0 d_0} & 0 & -\frac{(d_0 + x_0)}{C_0 d_0} \end{bmatrix} \begin{bmatrix} \delta x \\ \delta v \\ \delta q \end{bmatrix} + [0] \delta a$$

state:  $x = [\delta x, \delta v, \delta q]^T$

input:  $u = [\delta a]$  (acceleration)

output:  $y = [\delta e]$  (capacitor voltage)

# Accelerometer Transfer Function

```
>> A=[0 1 0;-10 -0.1 -(0.010595)/(0.01*0.1);-  
(0.010595)/(0.01*0.1) 0 -(0.1+0.005612)/(0.01*0.1)];  
>> B=[0;-1;0];  
>> C=[-(0.010595)/(0.01*0.1) 0 -(0.1+0.005612)/(0.01*0.1)];  
>> Gss=ss(A,B,C,0);  
>> G=tf(Gss)
```

Transfer function:

$$10.6 s + 3.367e-013$$

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 $s^3 + 105.7 s^2 + 20.56 s + 943.9$

```
>> zpk(G)
```

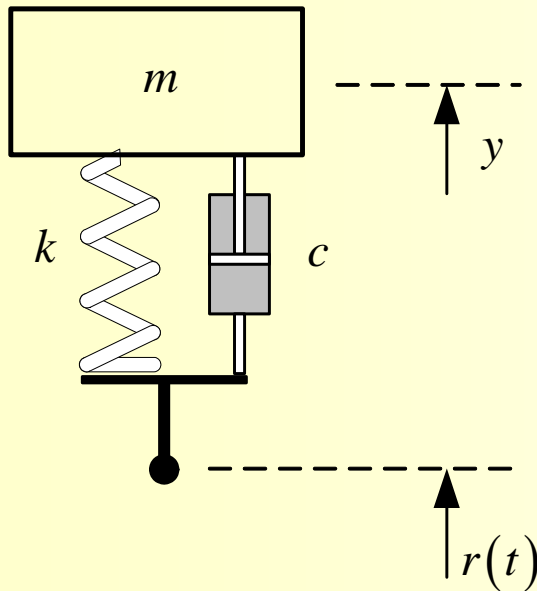
Zero/pole/gain:

$$10.595 s$$

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 $(s+105.6) (s^2 + 0.1101s + 8.938)$



# Reduction to State Space Form



$$m\ddot{y} = -k(y - r) - c(\dot{y} - \dot{r})$$

Try the usual:

$$\begin{aligned} x_1 &= y \\ x_2 &= \dot{x}_1 = \dot{y} \end{aligned} \Rightarrow \begin{aligned} \dot{x}_1 &= x_2 \\ \dot{x}_2 &= -\frac{k}{m}x_1 - \frac{c}{m}x_2 + \frac{k}{m}r + \frac{c}{m}\dot{r} \end{aligned}$$

An alternative:

$$\begin{aligned} x_1 &= y - \alpha_1 r \\ x_2 &= \dot{x}_1 - \alpha_2 \dot{r} \end{aligned} \Rightarrow \begin{aligned} y &= x_1 + \alpha_1 r \\ \dot{y} &= x_2 + \alpha_1 \dot{r} + \alpha_2 r \end{aligned}$$

$$\dot{x}_1 = x_2 + \alpha_2 r$$

$$\dot{x}_2 + \alpha_1 \dot{r} + \cancel{\alpha_2 \dot{r}} = -\frac{k}{m}(x_1 + \alpha_1 r) - \frac{c}{m}(x_2 + \cancel{\alpha_1 \dot{r}} + \alpha_2 r) + \frac{k}{m}r + \frac{c}{m}\dot{r}$$

$$\alpha_1 = 0 \text{ and } \alpha_2 = -\frac{c}{m}\alpha_1 + \frac{c}{m} \Rightarrow \alpha_1 = 0, \alpha_2 = \frac{c}{m}$$

$$\dot{x}_1 = x_2 + \frac{c}{m}r$$

$$\dot{x}_2 = -\frac{k}{m}x_1 - \frac{c}{m}x_2 + \left( -\left(\frac{c}{m}\right)^2 + \frac{k}{m} \right)r$$

# Computing Transfer Functions

From original equation:

$$m\ddot{y} = -k(y - r) - c(\dot{y} - \dot{r})$$

Use  $L[\dot{y}] = sL[y] - y(0) \Rightarrow L[\ddot{y}] = sL[\dot{y}] - \dot{y}(0) = s^2L[y] - sy(0) - \dot{y}(0)$

with  $y(0)=0$  and  $\dot{y}(0) = 0$

$$ms^2Y(s) = -kY(s) - csY(s) + kR(s) + csR(s)$$

$$Y(s) = \frac{cs + k}{ms^2 + cs + k} R(s) \Rightarrow G(s) = \frac{cs + k}{ms^2 + cs + k}$$

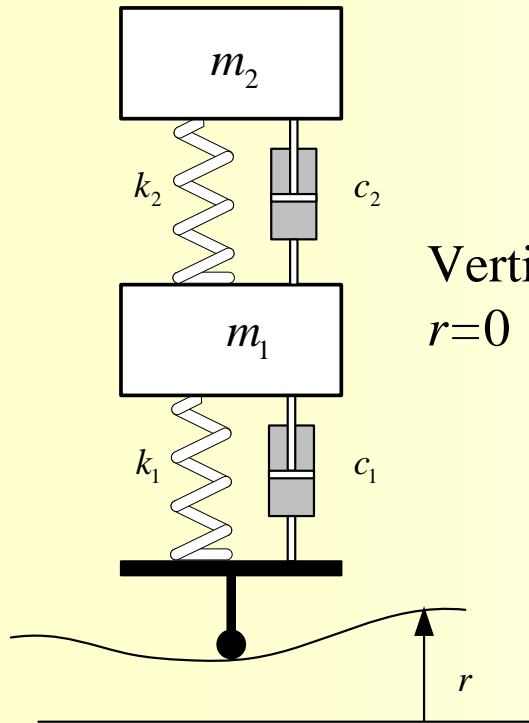
From state space

$$\frac{d}{dt} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -k/m & -c/m \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} c/m \\ (c/m)^2 + k/m \end{bmatrix} r, \quad y = \begin{bmatrix} 1 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 0 \end{bmatrix} r$$

$$G(s) = C[sI - A]^{-1} B + D = \begin{bmatrix} 1 & 0 \end{bmatrix} \begin{bmatrix} s & -1 \\ k/m & s + -c/m \end{bmatrix}^{-1} \begin{bmatrix} c/m \\ -(c/m)^2 + k/m \end{bmatrix} = \frac{cs + k}{ms^2 + cs + k}$$



# Quarter-Car Suspension



$$m_1 \ddot{y}_1 = -k_2(y_1 - y_2) - k_1(y_1 - r) - c_2(\dot{y}_1 - \dot{y}_2) - c_1(\dot{y}_1 - \dot{r})$$

$$m_2 \ddot{y}_2 = k_2(y_1 - y_2) + c_2(\dot{y}_1 - \dot{y}_2)$$

Verticle motion,  $y_1, y_2$  measured from rest with  $r=0$

Using Laplace Transform, derive a relationship between  $R(s)$  and  $Y_2(s)$  (data from Franklin et al)

$$Y_2(s) = \frac{(17.333/1.3067)s}{s^4 + 490s^3 + 44067.5s^2 + 157061s + 1.88099} R(s)$$



# Quarter-Car State Space Model

$$\frac{d}{dt} \begin{bmatrix} x_1 \\ v_1 \\ x_2 \\ v_2 \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 & 0 \\ -\frac{(k_1+k_2)}{m_1} & -\frac{c_1+c_2}{m_1} & \frac{k_2}{m_1} & \frac{c_2}{m_1} \\ 0 & 0 & 0 & 1 \\ \frac{k_2}{m_2} & \frac{c_2}{m_2} & -\frac{k_2}{m_2} & -\frac{c_2}{m_2} \end{bmatrix} \begin{bmatrix} x_1 \\ v_1 \\ x_2 \\ v_2 \end{bmatrix} + \begin{bmatrix} \frac{c_1}{m_1} \\ -(c_1+c_2)\frac{c_1}{m_1} + \frac{k_1}{m_1} \\ 0 \\ \frac{c_2 c_1}{m_1} \end{bmatrix} r(t)$$

$$y(t) = [0 \quad 0 \quad 1 \quad 0] \begin{bmatrix} x_1 \\ v_1 \\ x_2 \\ v_2 \end{bmatrix}$$

# Summary

- Accelerometer model
  - Start with physical principles
  - Nonlinear ordinary differential equations
  - First order form: ‘standard form’ or ‘state variable form’
- State space and transfer functions
- Solving ODEs / Transfer Functions
  - Linear systems are described by state space and transfer function models
  - Linear systems of ODEs can be solved using Laplace transforms
  - The transfer function is used to describe the input-output response
- Using MATLAB to solve odes
- Using MATLAB to compute transfer functions